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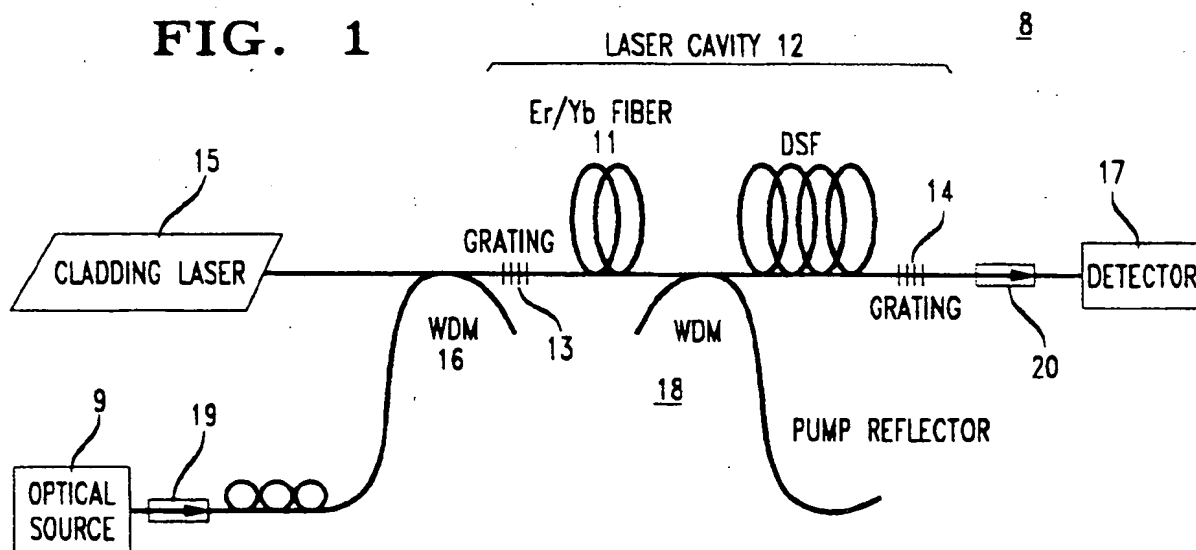
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(54) Intra-cavity optical four-wave mixer and optical communications system using the same

(57) An optical four-wave mixer for producing a phase-conjugated signal comprises a source of optical input signals, a fiber laser for receiving the signals, and a detector for selectively detecting the frequency-shifted signals produced by four-wave mixing. The laser can be a rare-earth doped fiber laser with a fiber cavity phase matched to the input signals. The frequency-shifted out-

put signals have an inverted spectral waveform as compared with the input signals. The mixer can be made in compact form with a cavity length as small as 100 m and can provide inverted signals at the same intensity as the input signals, making the mixer particularly useful for providing spectral inversion in an optical communications system.

FIG. 1



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## Description

### Field of the Invention

This invention relates to a device for efficient optical four-wave mixing. It is particularly useful for reversing the effect of dispersion in an optical communications systems.

### Background of the Invention

Optical communications systems are becoming increasingly important in the high speed transmission of large amounts of information. A typical optical communications system comprises a source of modulated optical input signals, a length of optical fiber coupled to the source, and a receiver for optical signals coupled to the fiber. The input signals are typically in the form of digital pulses which are transmitted with minimum attenuation in guided modes along the axis of the fiber.

One difficulty with optical communications systems is dispersion. Different wavelength components of a pulse are transmitted with slightly different facility with the consequence that a sharp, symmetrical pulse at the input, after traveling many kilometers, becomes deformed and unsymmetrical. In the absence of preventative measures, a pulse will eventually degrade to a point where its initial location in a binary sequence is indeterminate.

It has been proposed that dispersion can be reduced by midspan spectral inversion of propagating pulses, i.e. at the midpoint of the fiber path inverting the pulse waveform so that the higher frequency portion has the shape of the lower frequency portion and *vice versa* (effectively a 180° rotation of the pulse waveform about its center wavelength). As a result, after the inverted pulse travels over the second half of the communications path, the additional dispersion will reverse much of the distorting effect of the dispersion that occurred during the first half.

One approach to spectral inversion is through the use of a phenomenon known as four-wave mixing. When the pulse is co-propagated along a fiber with high power (5-50 mW) narrow band light near the pulse wavelength, a second pulse is produced at a wavelength slightly different from the original pulse. The frequency-shifted second pulse has an inverted waveform as compared to the initial pulse. Unfortunately, the four-wave mixing arrangements heretofore known require tens of kilometers of co-propagation and produce inverted pulses 10-25 dB down from the input pulse. Accordingly, there is a need for an improved four-wave mixer providing a stronger inverted pulse in a more compact arrangement.

### Summary of the Invention

An optical four-wave mixer for producing a phase-

conjugated signal comprises a source of optical input signals, a fiber laser for receiving the signals, and a detector for selectively detecting the frequency-shifted signals produced by four-wave mixing. The laser can be a rare-earth doped fiber laser with a fiber cavity phase matched to the input signals. The frequency-shifted output signals have an inverted spectral waveform as compared with the input signals. The mixer can be made in compact form with a cavity length as small as 100 m and can provide inverted signals at the same intensity as the input signals, making the mixer particularly useful for providing spectral inversion in an optical communications system.

### Brief Description of the Drawings

In the drawings:

FIG. 1 is a schematic diagram of an optical four-wave mixer in accordance with one embodiment of the invention;

FIG. 2 is a spectral diagram showing the various optical signals associated with the operation of the device of FIG. 1; and

FIG. 3 is a schematic diagram of an optical communications system employing the device of FIG. 1 for spectral inversion.

### Detailed Description

Referring to the drawings, FIG. 1 is a schematic diagram of an optical four-wave mixer 8 comprising a source 9 of optical input signals of center wavelength  $\lambda$ , a fiber laser 9 for receiving the input signals, and, a detector 17 provided downstream of the laser for selectively responding to the frequency-shifted four-wave mixing signals produced in the laser cavity. In typical applications the source will provide a digitally modulated sequence of input pulses at a constant repetition rate.

The laser can be composed of a rare-earth doped fiber 11, a laser cavity 12 defined by a pair of fiber Bragg gratings 13 and 14 and a pumping source 15. In this particular embodiment, a coupler 16 is provided for supplying input optical signals to the laser, and a coupler-reflector arrangement 18 is provided for reflecting pump radiation back through the rare-earth doped fiber. The center wavelength of the laser should be different from the signal wavelength  $\lambda$  so that the input signal, the laser light, and the mixing signal can all be separated, but the laser wavelength should also be within  $\pm 10\%$  of  $\lambda$ . Isolators 19 and 20 are advantageously provided to prevent reflection back into the input source and the laser cavity.

Preferably, the rare-earth doped fiber is Er/Yb fiber, the pumping source is a 1060 nm Nd cladding laser, and the laser cavity comprises 100 m to 5 Km of dispersion shifted fiber. The Bragg gratings can be two 0.5 nm wide fiber grating reflectors tuned to resonate at the minimum dispersion wavelength (1535 nm) of a 1 Km length of

dispersion shifted fiber. The detector can utilize a Fabry-Perot filter to selectively transmit the mixing pulses. For maximum conversion efficiency, the cavity is phase matched with the input signals as by choosing the minimum dispersion wavelength of the cavity fiber equal to the input wavelength  $\lambda$ .

In typical operation, a sequence of input pulses at a constant repetition rate are fed into the laser cavity. The laser output, prior to filtration, includes the input pulses, laser light, and four-wave mixing pulses which are inverted (conjugated) as compared with the input pulses and frequency-shifted to the other side of the laser light in a spectral diagram.

The device can be operated with the laser in either continuous wave operation or with the cavity adapted for mode-locked operation. For an input pulse source, the laser is preferably mode-locked at a repetition rate equal to the input pulse repetition rate, some integral multiple  $n$  of the repetition rate, or some integral fraction  $1/n$  of the repetition rate. In the continuous wave case, each input signal will generate a four-wave mixed output signal. In the mode-locked case, there can be a mixed pulse for each input pulse or for every  $n$ th pulse.

FIG. 2 is a spectral diagram of unfiltered output showing an input signal A, the laser light B and the conjugated output signal C. While the input signal here is at a longer wavelength than the laser, it can also be at a shorter wavelength. In general, when propagating through the erbium fiber prior to the dispersion shifted fiber, higher conversion efficiency is gained when the input signal is on the long wavelength side of the laser. When the input signal propagates through the dispersion shifted fiber first, the conversion efficiency is greater for an input signal on the short wavelength side of the laser. In general, the greater the frequency shift, the lower the conversion efficiency. The highest conversion efficiency was observed for an input signal traveling through the Yb/Er first, with 1060 nm pump power of 2.4 watts. Conjugate conversion efficiency as high as 0 dB was observed for a shift of 9.8 nm.

FIG. 3 is a schematic diagram of the preferred use of the FIG. 1 device for the spectral inversion of propagating signals in an optical communications system. Specifically, FIG. 3 illustrates an optical communication's system comprising a source 30 of modulated optical input signals, a first optical path 31, such as a length of optical fiber and a second optical path 32 through a similar optical medium to receiver 33 of optical signals. Disposed between similar, approximately equal optical paths is a four-wave mixing device 34 of the type shown in FIG. 1 for conjugating the spectral form of propagating signals. The effects of dispersion in the path from 31 are thus inverted, and these effects are essentially reversed as the conjugated pulses travel over a similar path 32 to the receiver. The receiver is adapted for selectively detecting the frequency-shifted, conjugated signals produced by four-wave mixing.

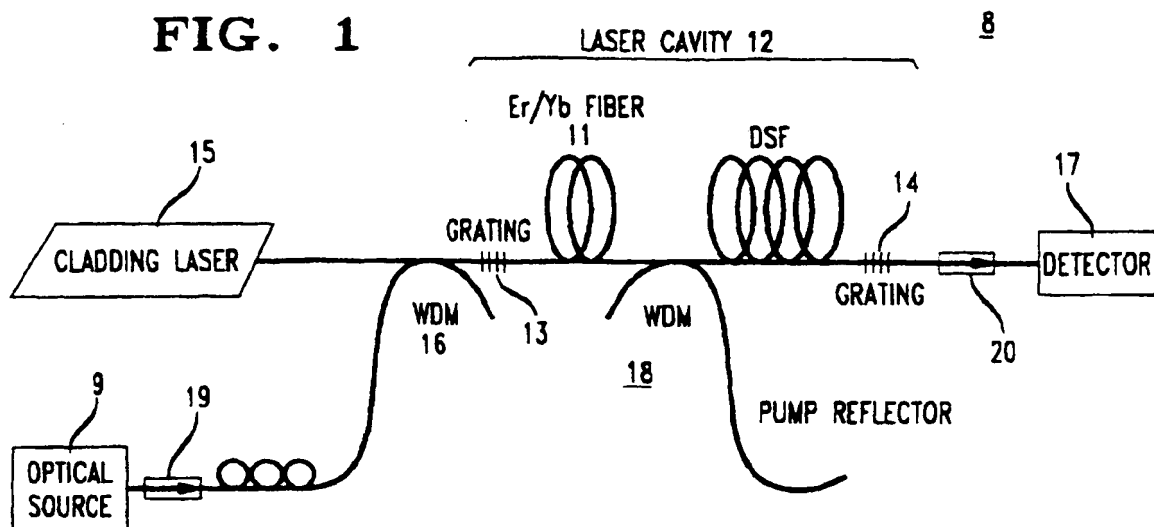
The subject four-wave mixing device can also be

modified for parametric amplification of the input signals. In this instance, the detectors, or receivers of the system are adapted to selectively utilize the amplified signal of wavelength  $\lambda$  (peak A of FIG. 2) rather than the conjugate signal (peak C).

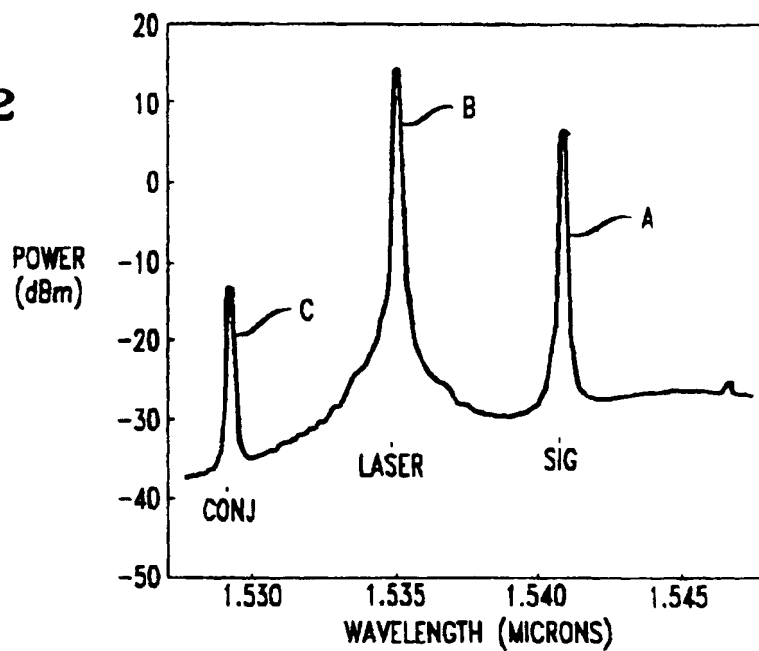
## Claims

1. An optical four-wave mixing device comprising:
  - a source of input signals of center wavelength  $\lambda$ ;
  - a rare-earth doped fiber laser for receiving said input signals, said fiber laser including a fiber cavity and adapted to generate light at a wavelength within 10% of  $\lambda$ ; and
  - a detector for selectively detecting frequency-shifted signals produced by said laser in response to said input signals by four-wave mixing.
2. A mixing device according to claim 1 wherein said fiber cavity comprises a length of fiber in the range 100 m to 5 Km.
3. A mixing device according to claim 1 wherein said fiber cavity comprises dispersion-shifted fiber.
4. A mixing device according to claim 1 wherein said fiber cavity is phase matched with said input signals.
5. A communications system comprising a source of optical signals, a pair of optical paths for propagating said signals, said paths having substantially equal dispersion effects on said signals, and disposed between said optical paths, a four-wave mixing device according to claim 1.
6. A device according to claim 1 wherein said source provides signal pulses at a repetition rate and said laser is mode-locked to said repetition rate, some integral multiple thereof, or some integral fraction thereof.
7. A device according to claim 1 wherein said detector comprises a filter for selectively permitting passage of said frequency-shifted signals.

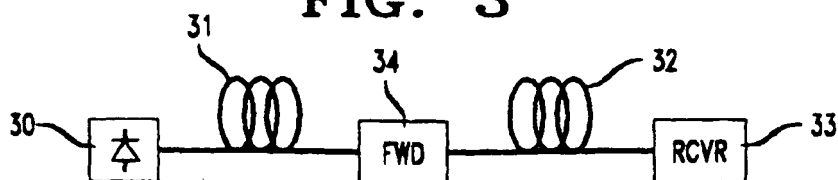
**FIG. 1**

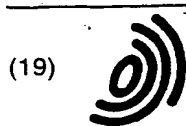


**FIG. 2**



**FIG. 3**





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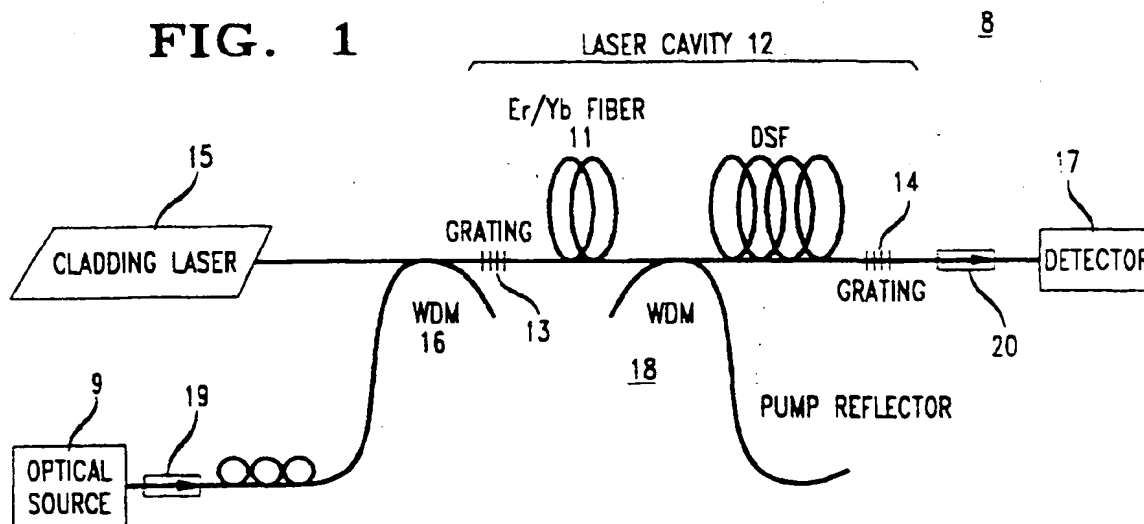
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FIG. 1





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# EUROPEAN SEARCH REPORT

Application Number  
EP 96 30 1146

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A	IEEE PHOTONICS TECHNOLOGY LETTERS, vol. 5, no. 10, 1 October 1993, pages 1241-1243, XP000414224 WATANABE S ET AL: "COMPENSATION OF PULSE SHAPE DISTORTION DUE TO CHROMATIC DISPERSION AND KERR EFFECT BY OPTICAL PHASE CONJUGATION" * figure 2 *	1-7	
A	EP 0 500 357 A (NIPPON ELECTRIC CO) 26 August 1992 * abstract *	1,5	
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The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 27 June 1997	Examiner Galanti, M
<p><b>CATEGORY OF CITED DOCUMENTS</b></p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons &amp; : member of the same patent family, corresponding document</p>			

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